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(54) **VALVE SWITCHING CONTROLS FOR
ADJUSTABLE DAMPER**

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CPC **F16F 9/464** (2013.01); **B60G 13/00**
(2013.01); **B60G 17/015** (2013.01); **B60G**
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B60G 17/0152; B60G 17/01908; F16F 9/464;
F16F 9/463
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See application file for complete search history.

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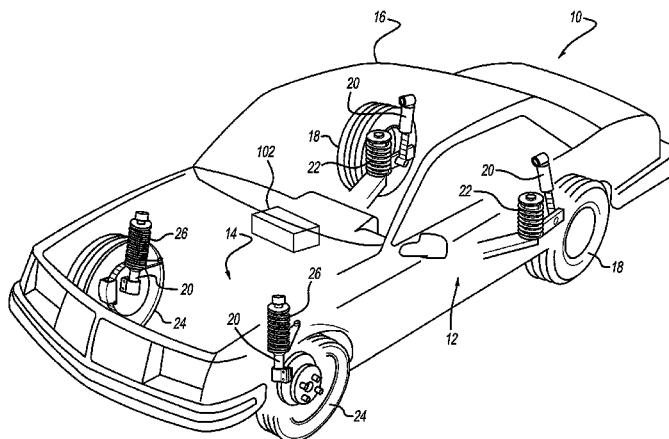
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(57) **ABSTRACT**

A damper system for a vehicle includes a shock absorber and
a damper module. The shock absorber includes a plurality of
digital valves. The shock absorber is operable at one of mul-
tiple damping states based on a valve state of the digital
valves. The damper module is coupled to each of the digital
valves and controls each of the digital valves to a desired state
based on a damper setting. The damper module determines a
target damping state, where the target state is one of the
multiple damping states. The damper module performs a
switch operation to control the valve state of the plurality of
digital valves to a given desired state when the target damping
state is different from a present damping state.

20 Claims, 13 Drawing Sheets



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CPC **B60G17/08** (2013.01); **F16F 9/3207**
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9/463 (2013.01); **B60G 2202/24** (2013.01);
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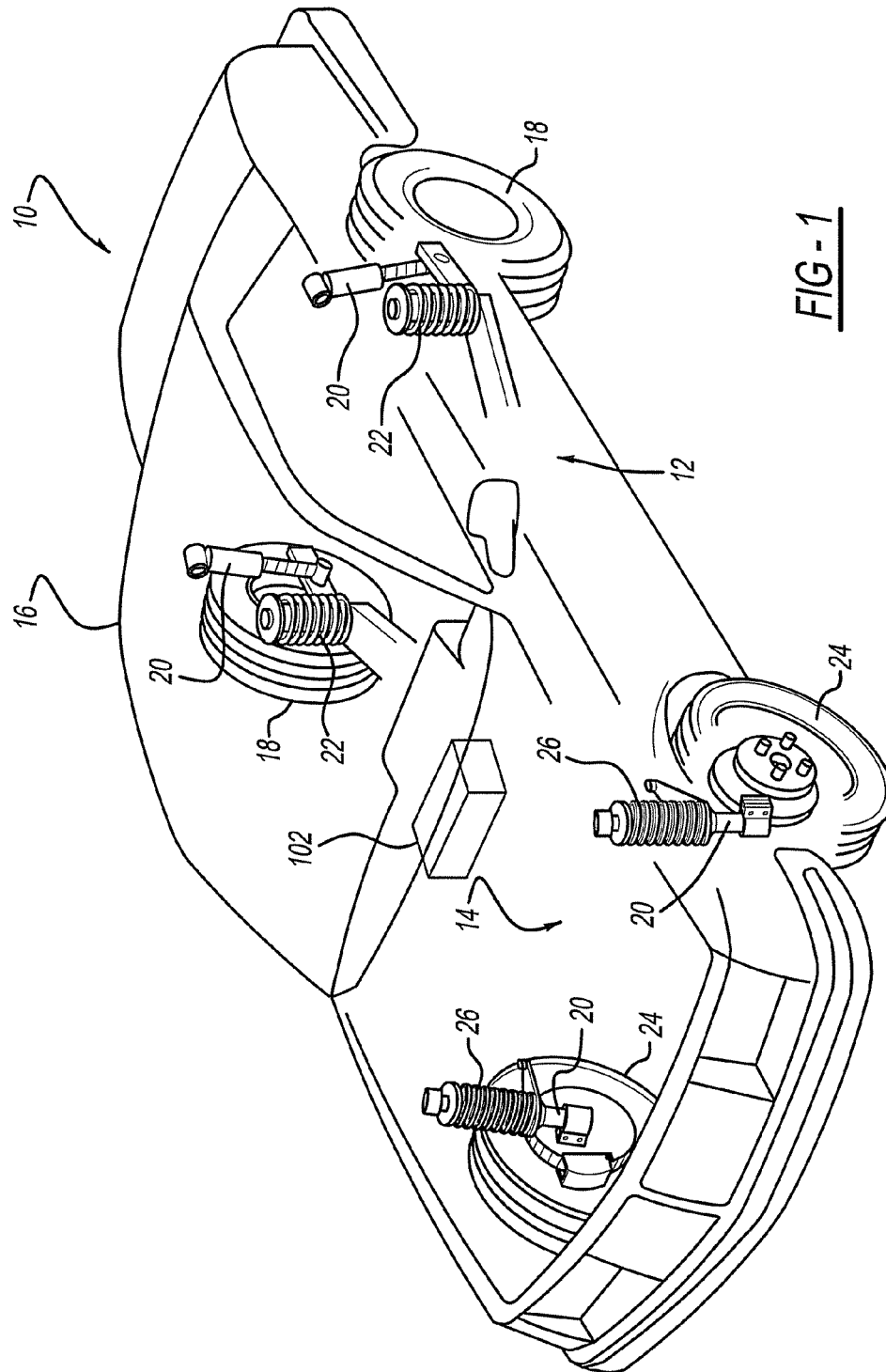
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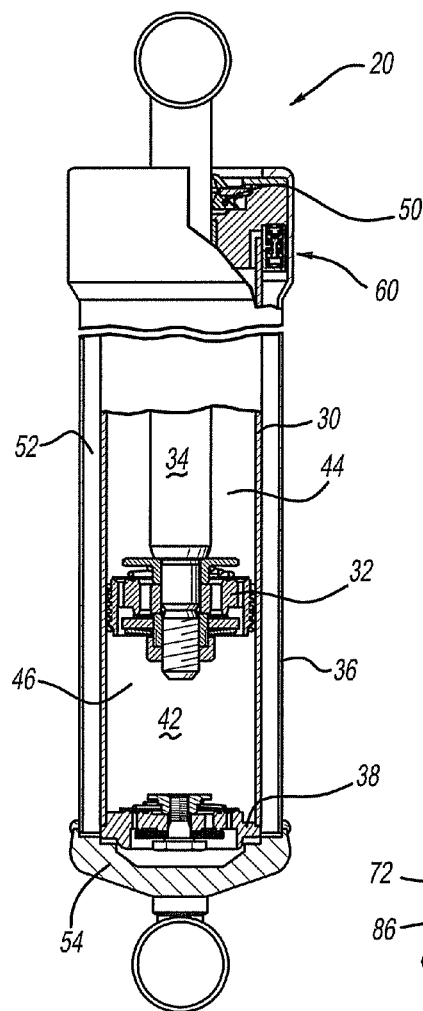


FIG - 2

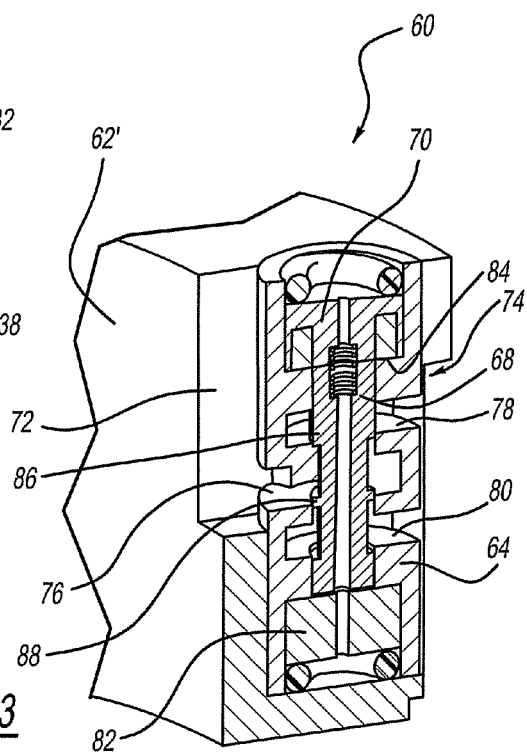
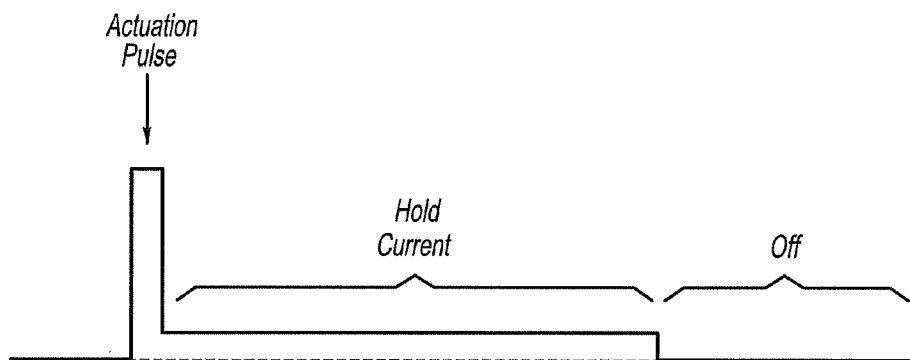
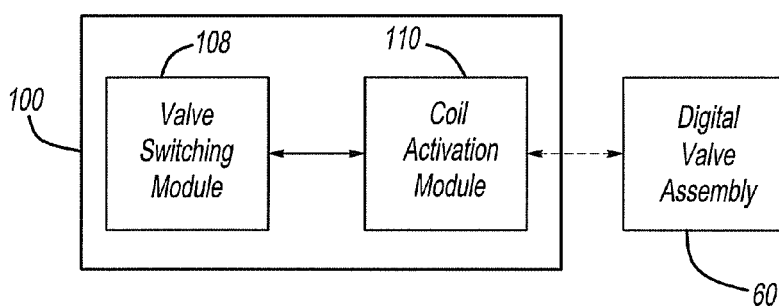
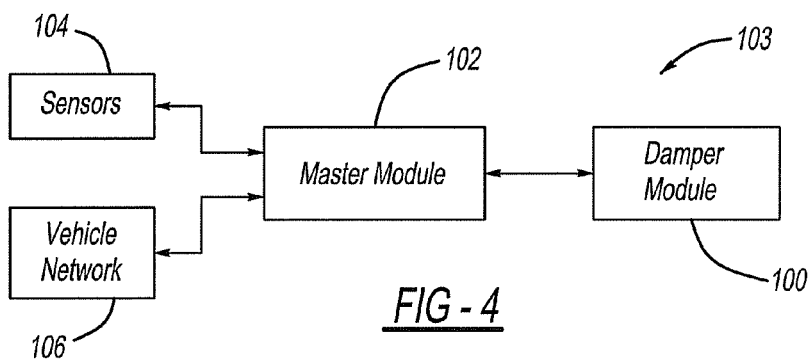
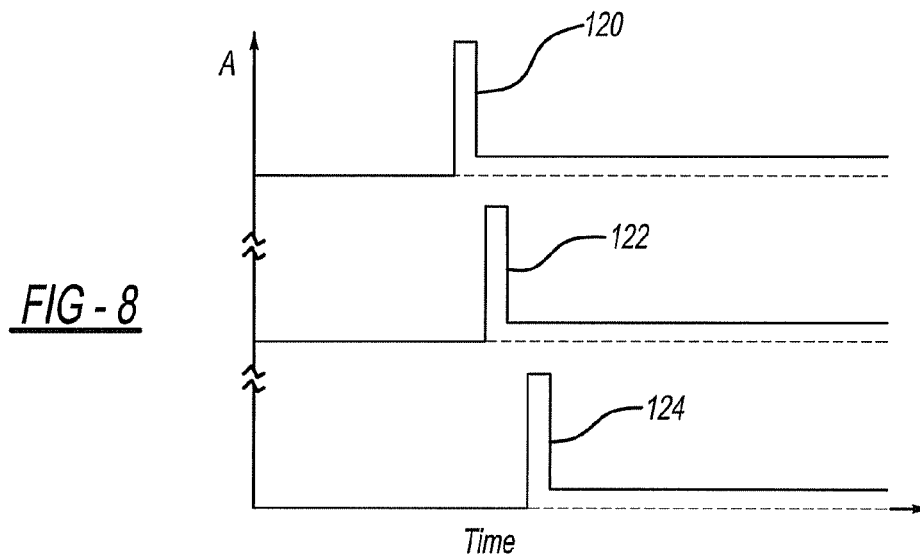


FIG - 3



Valve Position				Damping State
#1	#2	#3	#4	
OFF	OFF	OFF	OFF	1
OFF	OFF	OFF	ON	2
OFF	OFF	ON	OFF	3
OFF	OFF	ON	ON	4
OFF	ON	OFF	OFF	5
OFF	ON	OFF	ON	6
OFF	ON	ON	OFF	7
OFF	ON	ON	ON	8
ON	OFF	OFF	OFF	9
ON	OFF	OFF	ON	10
ON	OFF	ON	OFF	11
ON	OFF	ON	ON	12
ON	ON	OFF	OFF	13
ON	ON	OFF	ON	14
ON	ON	ON	OFF	15
ON	ON	ON	ON	16

FIG - 6

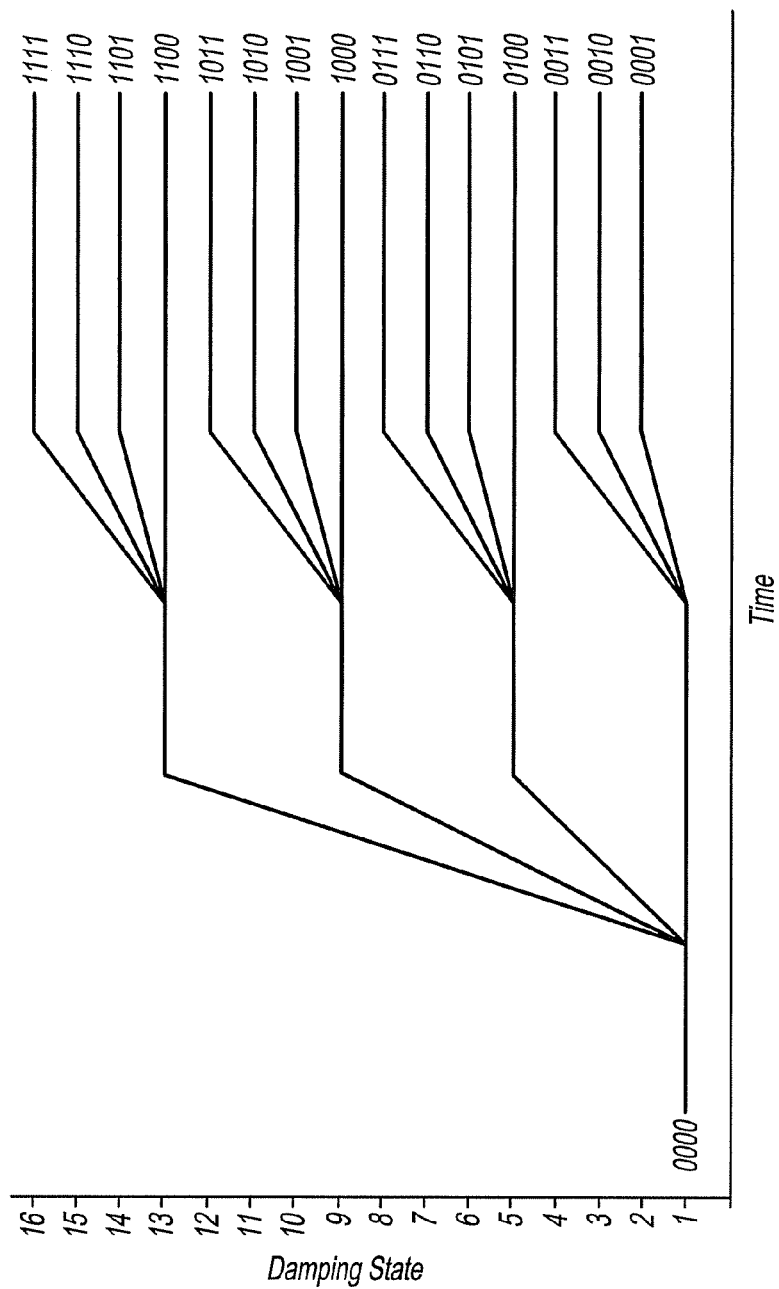


FIG - 9

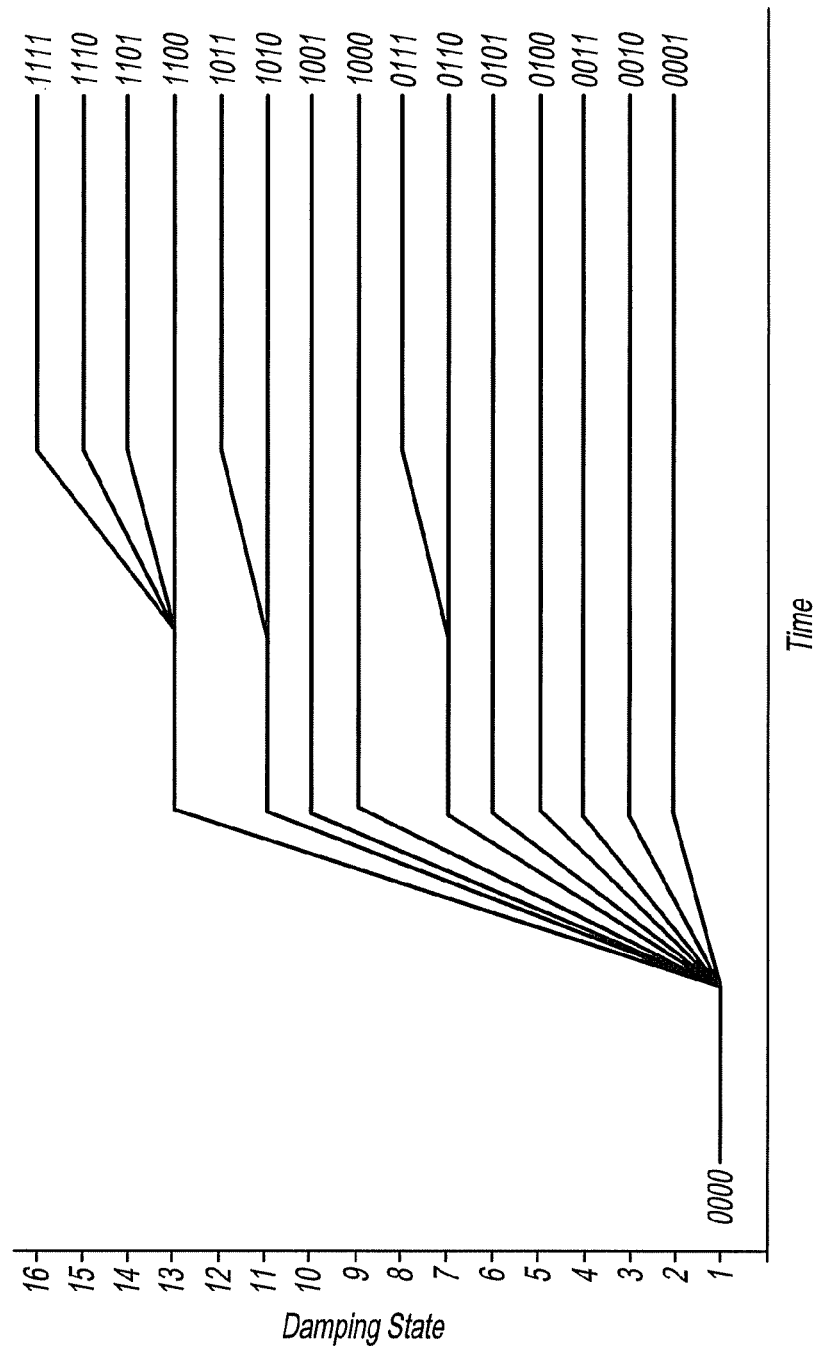


FIG - 10

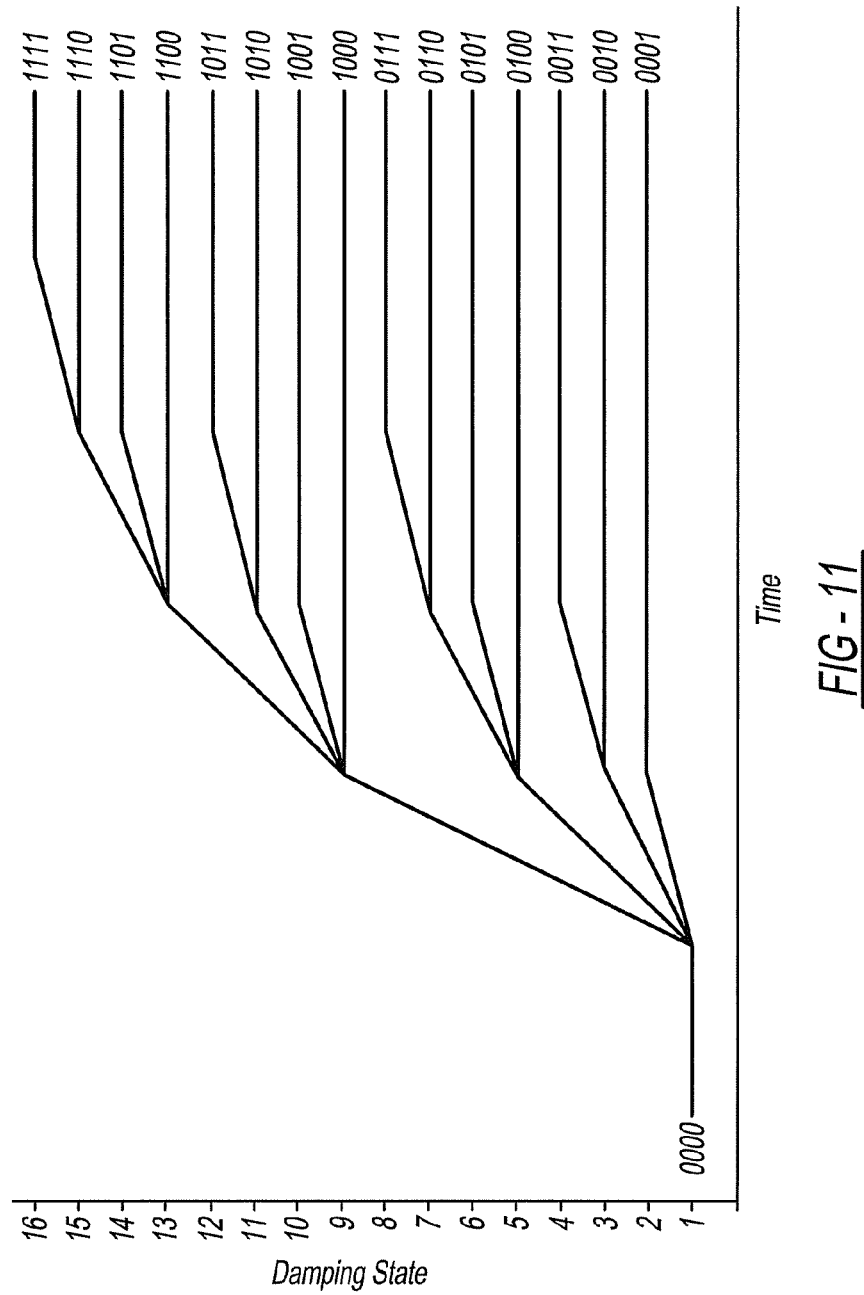


FIG - 11

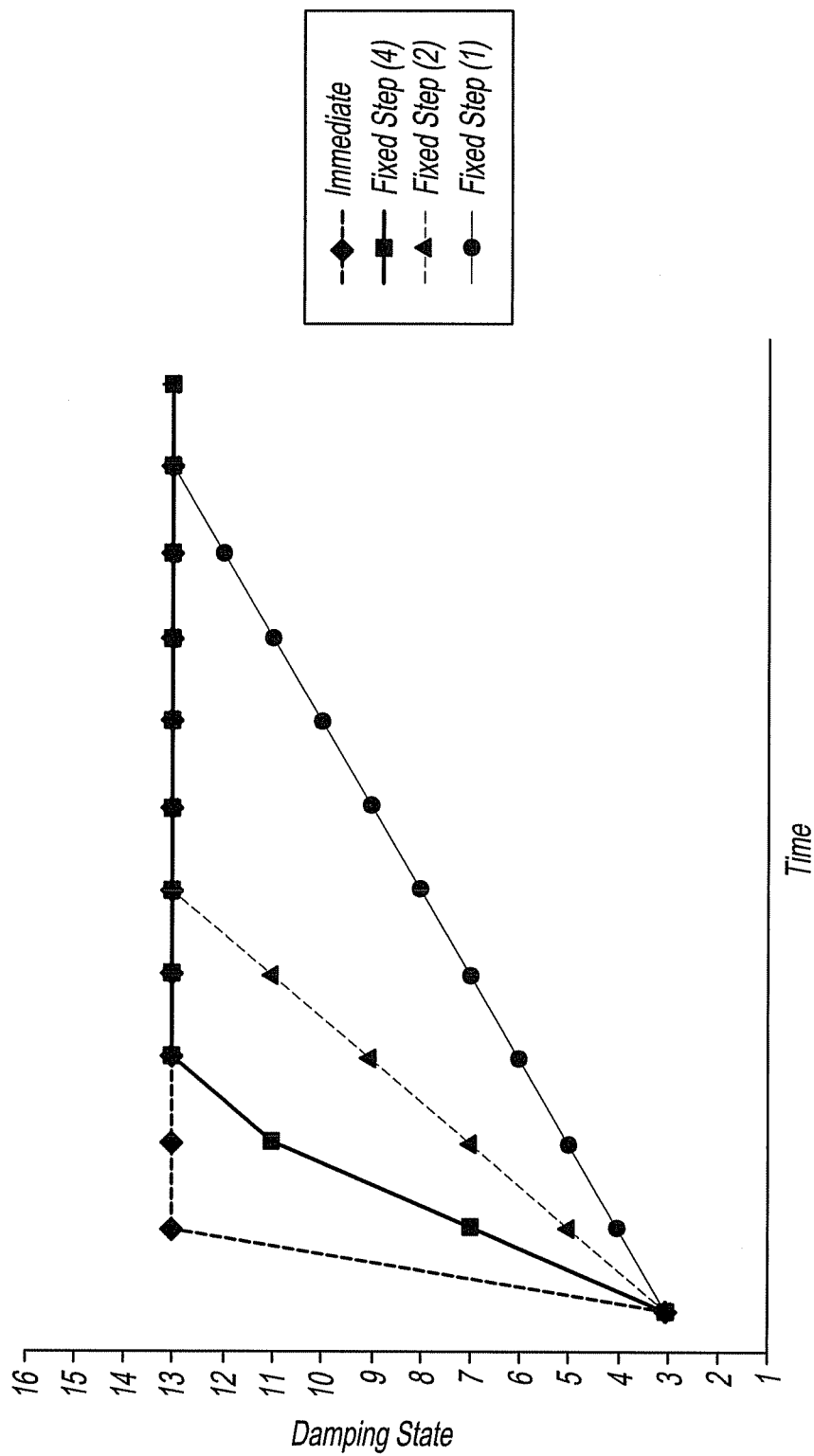
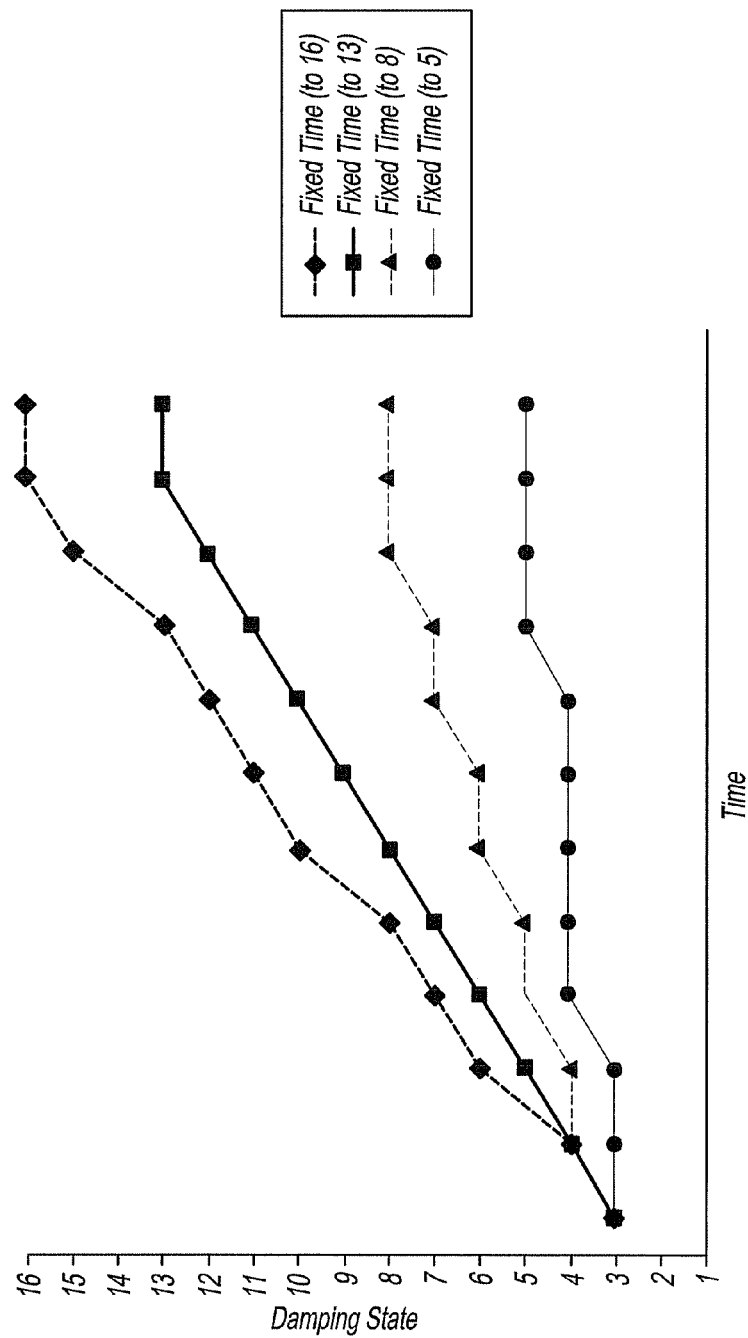


FIG - 12



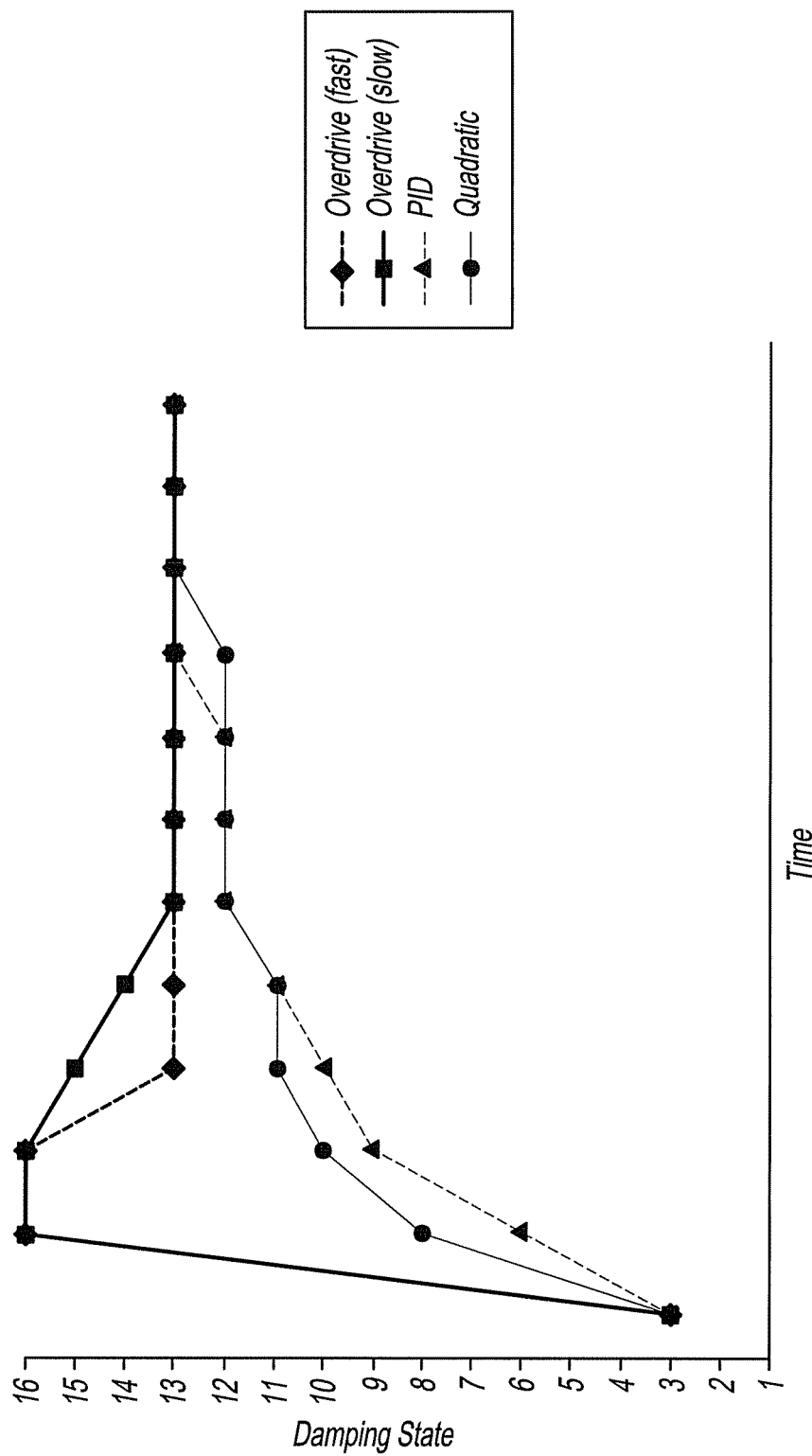


FIG - 14

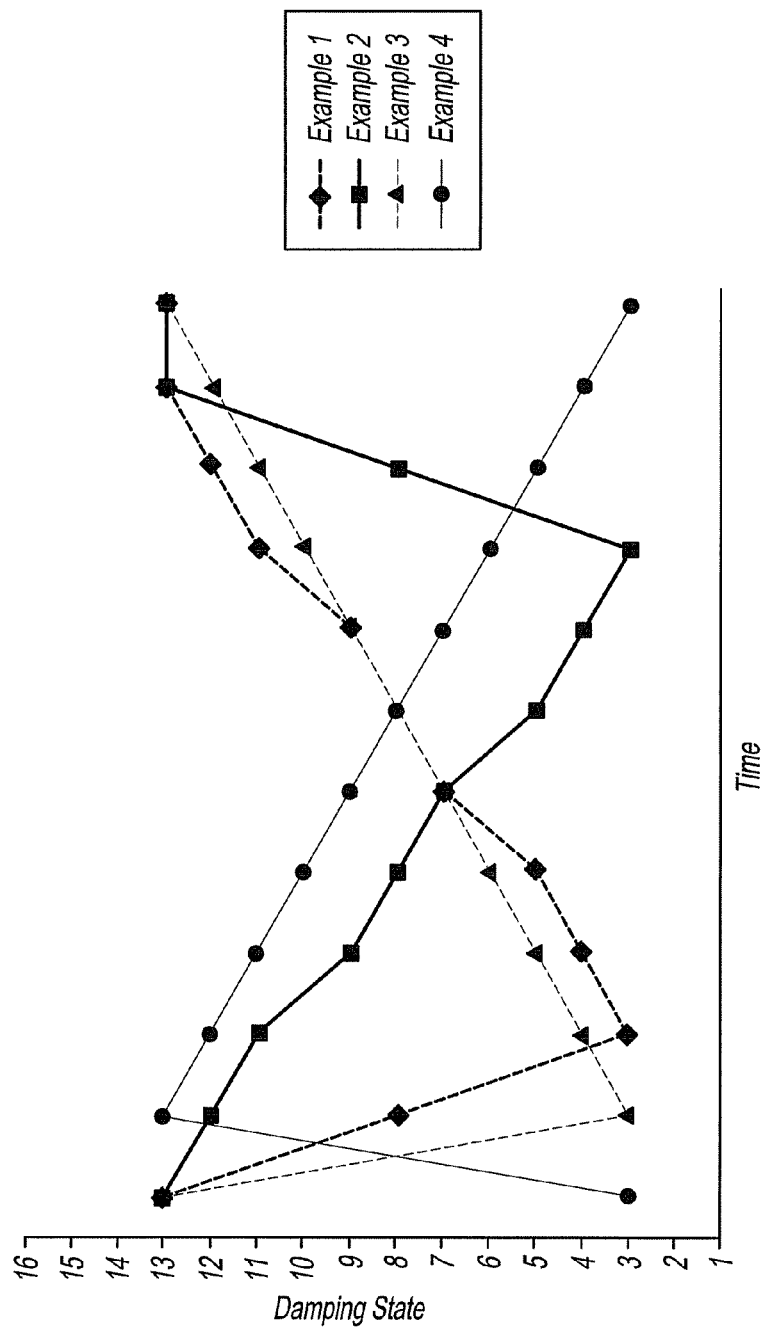
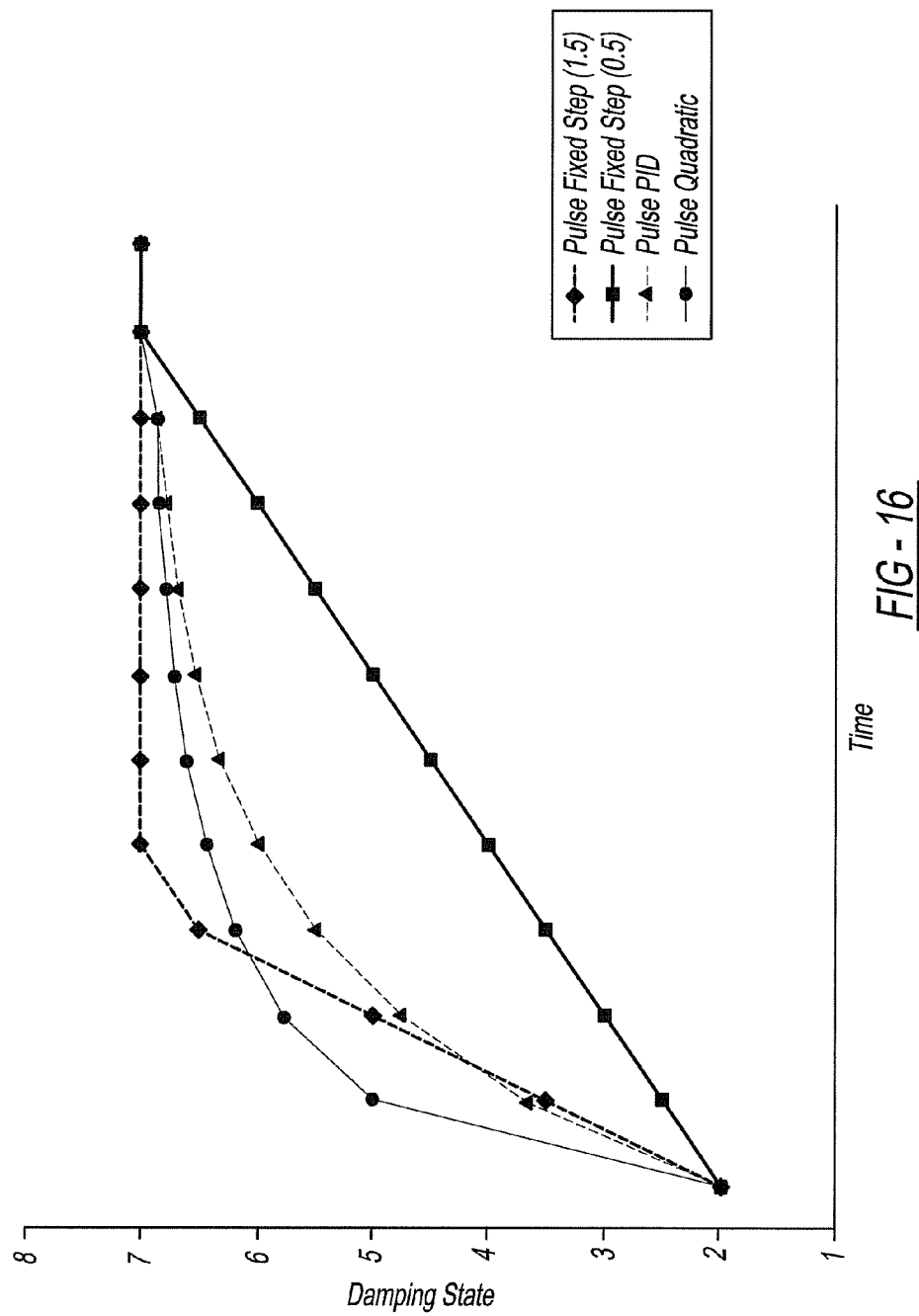
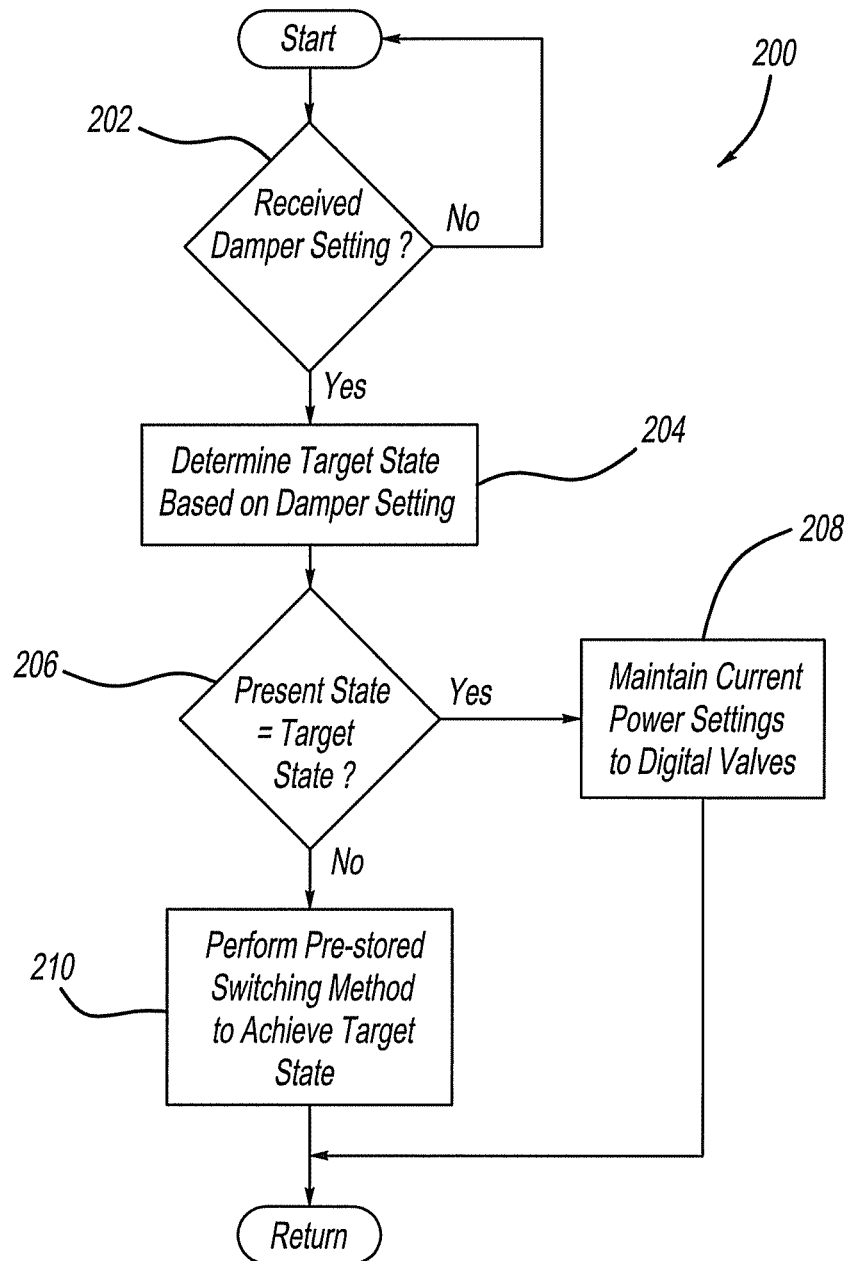


FIG - 15



FIG - 17

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VALVE SWITCHING CONTROLS FOR ADJUSTABLE DAMPER

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims the benefit of U.S. Provisional Application No. 61/770,426, filed on Feb. 28, 2013. The entire disclosure of the above application is incorporated herein by reference.

FIELD

The present disclosure relates to an electrically adjustable damper having one or more digital valves. More particularly, to a valve switching control for adjusting a damping state of the electrically adjustable damper.

BACKGROUND

This section provides background information related to the present disclosure which is not necessarily prior art.

Shock absorbers are used in conjunction with automotive suspension systems to absorb unwanted vibrations which occur during driving. To absorb the unwanted vibrations, shock absorbers are generally connected between the sprung portion (body) and the unsprung portion (suspension) of the automobile.

In recent years, vehicles may be equipped with an electrically adjustable damping system that includes an adjustable shock absorber having a digital valve. More particularly, the adjustable shock absorber may include an electromechanical coil or solenoid disposed therein.

A master module which may be located on the vehicle body can be used to control a damping state of each of the adjustable shock absorber. For example, the master module may receive data from various sensors disposed along the sprung and unsprung portions of the vehicle. Based on the data received, the master module determines the damping state of the adjustable shock absorber and actuates the electromechanical coil/solenoid disposed within the shock absorber.

SUMMARY

This section provides a general summary of the disclosure, and is not a comprehensive disclosure of its full scope or all of its features.

The present disclosure provided for a damper system for a vehicle. The damper system includes a shock absorber and a damper module. The shock absorber includes a plurality of digital valves, where each digital valve has a valve state. The shock absorber is operable at one of multiple damping states based on the valve state of the plurality of digital valves;

The damper module is coupled to each of the digital valves and controls each of the digital valves to a desired state based on a damper setting received from a master module. The damper module determines a target damping state of the shock absorber based on the damper setting. The target damping state is one of the multiple damping states. The damper module performs a switch operation to control the valve state of the plurality of digital valves to a given desired state when the target damping state is different from a present damping state.

Further areas of applicability will become apparent from the description provided herein. The description and specific

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examples in this summary are intended for purposes of illustration only and are not intended to limit the scope of the present disclosure.

DRAWINGS

The drawings described herein are for illustrative purposes only of selected embodiments and not all possible implementations, and are not intended to limit the scope of the present disclosure.

FIG. 1 is an illustration of a vehicle having an adjustable shock absorber;

FIG. 2 is a partial cross-sectional view of the shock absorber;

FIG. 3 is an enlarged partial cross-sectional view of a digital valve assembly disposed in the shock absorber;

FIG. 4 is an example functional block diagram of a vehicle damper system;

FIG. 5 is an example functional block diagram of a damper module;

FIG. 6 illustrates a correlation between a damping state and a valve state for each digital valve assembly of a shock absorber having four digital valve assemblies;

FIG. 7 illustrates an actuation pulse, a hold current, and an off-current;

FIG. 8 illustrates a staggering control of three actuation pulses;

FIG. 9 is a graph of an example operation of a basic delay staggering for a valve staggering control;

FIG. 10 is a graph of an example operation of a smart delay staggering for the valve staggering control;

FIG. 11 is a graph of an example operation of a flow-area staggering for the valve staggering control;

FIG. 12 is a graph of an example operation of a fixed-step control for a state transition control;

FIG. 13 is a graph of an example operation of a fixed-time control for the state transition control;

FIG. 14 is a graph of an example operation of an overdrive control, a PID control, and quadratic control for the state transition control;

FIG. 15 is a graph of an example operation of an asymmetrical control for the state transition control;

FIG. 16 is a graph of pulse mode operation control for the state transition control; and

FIG. 17 is a flow chart of an example method for performing a valve switching operation.

Corresponding reference numerals indicate corresponding parts throughout the several views of the drawings.

DETAILED DESCRIPTION

Example embodiments will now be described more fully with reference to the accompanying drawings.

The following description is merely exemplary in nature and is not intended to limit the present disclosure, application, or uses. With reference to FIG. 1, an example of a vehicle 10 incorporating a suspension system having shock absorbers, each of which incorporate a digital valve is now presented. The vehicle 10 includes a rear suspension 12, a front suspension 14 and a body 16. The rear suspension 12 has a transversely extending rear axle assembly (not shown) adapted to operatively support a pair of rear wheels 18. The rear axle is attached to the body 16 by means of a pair of shock absorbers 20 and by a pair of springs 22.

Similarly, the front suspension 14 includes a transversely extending front axle assembly (not shown) to operatively

support a pair of front wheels **24**. The front axle assembly is attached to the body **16** by means of a pair of shock absorbers **20** and a pair of springs **26**.

The shock absorbers **20** serve to dampen the relative motion of the unsprung portion (i.e., front and rear suspensions **12, 14**) with respect to the sprung portion (i.e., body **16**) of vehicle **10**. While the vehicle **10** has been depicted as a passenger car having front and rear axle assemblies, the shock absorbers **20** may be used with other types of vehicles or in other types of applications including, but not limited to, vehicles incorporating non-independent front and/or non-independent rear suspensions, vehicles incorporating independent front and/or independent rear suspensions, or other suspension systems known in the art. Further, the term "shock absorber" as used herein is meant to refer to dampers in general and thus will include McPherson struts and other damper designs known in the art.

Referring now to FIG. 2, an example of the shock absorber **20** is shown in greater detail. The shock absorber **20** comprises a pressure tube **30**, a piston assembly **32**, a piston rod **34**, a reserve tube **36**, and a base valve assembly **38**. The pressure tube **30** defines a working chamber **42**. The piston assembly **32** is slidably disposed within the pressure tube **30** and divides the working chamber **42** into an upper working chamber **44** and a lower working chamber **46**.

The piston rod **34** is attached to the piston assembly **32** and extends through the upper working chamber **44** and through a rod guide assembly **50** which closes the upper end of the pressure tube **30**. The end of the piston rod **34** opposite to the piston assembly **32** is adapted to be secured to the sprung mass of the vehicle **10** in the non-inverted configuration.

Valving within the piston assembly **32** controls the movement of fluid between the upper working chamber **44** and the lower working chamber **46** during movement of the piston assembly **32** within the pressure tube **30**. Since the piston rod **34** extends only through the upper working chamber **44** and not the lower working chamber **46**, movement of the piston assembly **32** with respect to the pressure tube **30** causes a difference in the amount of fluid displaced in the upper working chamber **44** and the amount of fluid displaced in the lower working chamber **46**. The difference in the amount of fluid displaced is known as the "rod volume" and it flows through the base valve assembly **38**.

The reserve tube **36** surrounds the pressure tube **30** to define a fluid reservoir chamber **52** located between tubes **30** and **36**. The bottom end of the reserve tube **36** is closed by a base cup **54** which is adapted to be connected to the unsprung mass of vehicle **10** in the non-inverted configuration. The upper end of reserve tube **36** is attached to rod guide assembly **50**. The base valve assembly **38** is disposed between the lower working chamber **46** and the reservoir chamber **52** to control the flow of fluid between chambers **46** and **52**. When the shock absorber **20** extends in length, an additional volume of fluid is needed in the lower working chamber **46** due to the "rod volume" concept. Thus, fluid will flow from the reservoir chamber **52** to the lower working chamber **46** through the base valve assembly **38**. When shock absorber **20** compresses in length, an excess of fluid must be removed from the lower working chamber **46** due to the "rod volume" concept, and therefore, fluid will flow from the lower working chamber **46** to the reservoir chamber **52** through the base valve assembly **38**.

Alternatively, the shock absorber may be configured as an inverted shock absorber. As the inverted shock absorber, the end of the piston rod **34** opposite to the piston assembly **32** is

adapted to be secured to the unsprung mass of the vehicle **10** and the base cup **54** is adapted to be connected to the sprung mass of vehicle **10**.

With reference to FIG. 3, the shock absorber **20** includes a digital valve assembly **60**. For brevity, the digital valve assembly **60** may be referred to as the digital valve **60**. The digital valve **60** is a two position valve assembly which has a different flow area in each of the two positions. The digital valve **60** may include a valve housing **62**, a sleeve **64**, a spool **68**, and a coil assembly **70**.

The valve housing **62** defines a valve inlet **72** which is in communication with the upper working chamber **44** through a fluid passage (not shown) and a valve outlet **74** which is in fluid communication with the reservoir chamber **52**. The sleeve **64** is disposed within the valve housing **62**. The sleeve **64** defines an annular inlet chamber **76** which is in communication with the valve inlet **72** and a pair of annular outlet chambers **78** and **80** which are in communication with valve outlet **74**.

The spool **68** is slidably received within the sleeve **64** and axially travels within the sleeve **64** between the coil assembly **70** and a stop puck **82** disposed within the sleeve **64**. A spring may be used to bias the spool **68** away from the coil assembly **70** and towards the stop puck **82**. A shim **84** is disposed between the coil assembly **70** and the sleeve **64** to control the amount of axial motion for the spool **68**.

The spool **68** defines a first flange **86** which controls fluid flow between the annular inlet chamber **76** and the annular outlet chamber **78** and a second flange **88** that controls fluid flow between the annular inlet chamber **76** and the annular outlet chamber **80**. The flanges **86** and **88** thus control fluid flow from the upper working chamber **44** to the reservoir chamber **52**.

The coil assembly **70** is disposed within the sleeve **64** to control the axial movement of the spool **68**. The wiring connections for the coil assembly **70** can extend through a rod guide housing (not shown), through the sleeve **64**, through valve housing **62** and/or through the reserve tube **36**. When there is no power provided to the coil assembly **70**, the damping characteristics will be defined by the flow area of the digital valve **60** in its first position, the piston assembly **32** and the base valve assembly **38**.

The movement of spool **68** is controlled by supplying power to coil assembly **70** to move the digital valve **60** to its second position. The digital valve **60** can be kept in its second position by continuing to supply power to the coil assembly **70** or by providing means for retaining digital valve **60** in its second position and discontinuing the supply of power to the coil assembly **70**. The means for retaining the digital valve **60** in its second position can include mechanical means, magnetic means or other means known in the art. Once in its second position, movement to the first position can be accomplished by terminating power to the coil assembly **70** or by reversing the electrical current or reversing the polarity of the power supplied to the coil assembly **70** to overcome the retaining means.

The shock absorber **20** may include one or more digital valves **60**. When multiple digital valves **60** are used, the total flow area through the plurality of digital valves **60** can be set at a specific number of total flow areas depending on the position of each individual digital valve **60**. The specific number of total flow areas can be defined as being $2n$ flow areas where n is the number of digital valves **60**. For example, in the following description the shock absorber **20** is described as having four digital valves **60**. The number of total flow areas available would be 24 or sixteen flow areas, where each flow area influences the damping level of the

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shock absorbers 20. Accordingly, with four digital valves 60, the shock absorber 20 may be controlled to sixteen discrete and distinct level of damping, as described in further below.

Furthermore, when multiple digital valves 60 are used, the flow area of the digital valves may be varied. For example, if two digital valves 60 are used, one digital valve may have a larger flow area than the other digital valve. Accordingly, the flow area provided by the digital valve 60 may be customized by adjusting the orifice size of the digital valve 60.

Fluid flow through the digital valve 60 will occur both during a rebound or extension stroke and during a compression stroke. During a rebound or extension stroke, fluid in the upper working chamber 44 is pressurized, which then forces fluid flow through the digital valve 60 when it is opened. During a compression stroke, fluid flows from the lower working chamber 46 to the upper working chamber 44 through the piston assembly 32 due to the “rod volume” concept. When the digital valve 60 is opened, an open flow path between the upper working chamber 44 and the reservoir chamber 52 is created. Additional fluid flow will flow through the piston assembly 32 and through the digital valve 60 because this open flow path creates the path of least resistance to the reservoir chamber 52 in comparison to flow through the base valve assembly 38.

While in the example embodiment the digital valve assembly 60 is positioned at or near the rod guide assembly 50 of the shock absorber 20, the digital valve 60, may be positioned at other locations within the shock absorber 20. In particular, further details regarding the shock absorber 20 and the digital valve 60, is further described in Applicant’s commonly owned U.S. Pat. No. 8,616,351 for “Damper With Digital Valve” which issued Dec. 31, 2013, the disclosure of which is incorporated herein.

The shock absorber 20 further includes a damper module 100. The damper module 100 may be disposed with the shock absorber 20 in a separate housing (not shown). The damper module 100 controls the positions of the digital valves 60 disposed within the shock absorbers 20 to adjust the dampening characteristics of the shock absorber 20. The shock absorber 20 and the damper module 100 may be referred to together as a damping system.

The damper module 100 may receive a damper setting from a master module 102. The master module 102 is disposed in the vehicle 10 (FIG. 1). The master module 102 is communicably coupled to the damper module 100 of each of the shock absorbers 20 disposed in the vehicle 10.

With reference to FIG. 4, an example of a vehicle damper system 103 is shown. The master module 102 receives data from various sensors 104 disposed at or near the shock absorbers 20 and/or disposed at other positions of the vehicle 10. The sensors 104 may include but are not limited to an angular rate sensor, an inertial measurement unit (IMU), a temperature sensor, a height sensor, a pressure sensor, an accelerometer, and other suitable sensors that provide data used for controlling the dampening characteristics of the shock absorber 20.

The master module 102 may also receive information from other modules disposed in the vehicle 10 via a vehicle network 106. The vehicle network 106 may be a controller area network (CAN), a local interconnect network (LIN), or other suitable networks. The master module 102 may receive for example, information regarding the rotation of the steering wheel from a steering wheel position sensor via the vehicle network 106.

Based on the inputs received, the master module 102 determines a damper setting for each of the shock absorbers 20. Specifically, the master module 102 may include a series of

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algorithms in the form of computer executable programs that determine the damper setting based on the inputs received. The damper setting is provided to the damper module 100 of each of the shock absorbers 20. In addition, the master module 102 may provide the information received from the sensors 104 and/or the vehicle network 106 to the damper module. For example, the damper module 100 may receive data related to the temperature of the shock absorber or an acceleration of the vehicle. In the example embodiment the master module 102 is disposed separately from the damper module 100. Alternatively, the master module 102 may be disposed with the damper module 100, such that each damper module 100 includes a master module.

With reference to FIG. 5, an example of the damper module 100 is presented. The damper module 100 may include a valve switching module 108 and a coil activation module 110. Based on the damper setting, the valve switching module 108 determines a damping state of the shock absorber 20. For example, with four digital valves 60, the shock absorber 20 may have sixteen discrete and distinct levels of damping which range from soft to firm.

The valve switching module 108 may include a table that correlates the damping state with a position or valve state of each of the digital valves 60 provided in the shock absorber 20. For example, with reference to FIG. 6, the four digital valves 60 may be identified in the table as #1, #2, #3, and #4. For each of the damping states, the valve state of the digital valve 60 may be defined as “OFF” or “ON”. In an OFF-state the coil assembly 70 of the digital valve 60 does not receive power and is in the first position. Conversely, in an ON-state, the coil assembly 70 receives power such that the digital valve 60 is in the second position. As illustrated in FIG. 6, for a damping state, all of the digital valves 60 are in the OFF-state. Alternatively, to achieve a seventh damping state, the #1-digital valve 60 (#1) and the #4-digital valve 60 (#4) are in the OFF-state and the #2-digital valve 60 (#2) and #3-digital valve 60 (#3) are in the ON-state.

The damper setting received by the damper module 100 is a target state of the shock absorber 20. The valve switching module 108 compares the target state with a present state of the shock absorber 20 which is the present damping state of the shock absorber 20. If the target state is different from the present state, the valve switching module 108 may refer to the target state as a desired state.

Based on the target state and the present state, the valve switching module 108 determines a control operation of the digital valve 60. Specifically, the valve switching module 108 determines whether control operation of the digital valve 60 is in an actuation operation, a hold operation, or an off operation. With reference to FIG. 7, in the actuation operation of the digital valve 60, an electrical current pulse (i.e., actuation pulse) is applied to move the digital valve 60 from the first position to the second position via the coil assembly 70 (i.e., ON-state). Accordingly, the actuated position of the digital valve 60 can correspond to either the hydraulically opened or closed condition depending on the mechanical configuration of the digital valve 60.

During the hold operation, an electrical current pulse having a lower steady state level than the actuation pulse can be applied to keep the digital valve 60 in the ON-state. Specifically, after the digital valve 60 is actuated, the hold operation can be performed to maintain the digital valve 60 in the ON-state. Alternatively, if the digital valve 60 includes a means for retaining the digital valve 60 in its second position, as described above, no electrical current pulse is applied to the coil assembly 70 during the hold operation.

The off-operation deactivates the digital valve 60. For example, current may no longer be provided to the digital valve 60. Accordingly, the digital valve 60 moves from the second position to the first position, and the digital valve 60 is in the OFF-state. Alternatively, if the digital valve 60 includes a means for retaining the digital valve 60 in its second position, as described above, during the off-operation a reverse current or reverse polarity of power may be supplied to the coil assembly 70 to overcome the retaining means.

The digital valve 60 of the shock absorber 20 is electrically coupled to the coil activation module 110 via the coil assembly 70 (represented by dotted line in FIG. 5). The valve switching module 108 provides the control operation to the coil activation module 110 which then operates the coil assembly 70 accordingly. For example, if the digital valve 60 is to be actuated, the coil activation module 110 provides the activation current pulse to the coil assembly 70 of the digital valve 60.

To provide a fast, smooth, and power efficient switching of the damper state from the present state to the desired state, the valve switching module 108 may control a switch time and/or transition period during which the digital valve 60 shifts from the present state to the desired state. Specifically, valve switching can be used to create a faster hydraulic response. The valve switching module 108 includes various types of switching methods to help alleviate delays inherent with fluid dynamics.

The switching methods may also minimize hydraulic pressure transients associated with changing the firmness setting during dynamic operation of the damper system. The switching methods are intended to provide smooth transitions during hydraulic changes in the damper system. Accordingly, vehicle noise, vibration, and harshness (NVH) can be optimized by utilizing the switching methods described here.

Furthermore, the peak current required for actuating the digital valves 60 can be reduced by utilizing the switching methods that minimize the number of digital valves 60 switched or by creating time offsets between actuation pulses. The switching methods provided by the valve switching module 108 may be separated into two categories: valve staggering control and state transition control.

The valve staggering control refers to a method in which a transient state may be used between the present state and the desired state. The transient state, which may also be referred to as transient intermediate state, is one or more damping states different from the present state and the desired state that are achieved prior to the desired state (i.e., the target state). One goal of the transient state is to reduce the peak current requirement. Specifically, short time delays (e.g., 1-2 milliseconds) may be added between the actuation operations of the digital valves 60. For example, as shown in FIG. 8, actuation pulses 120, 122, 124 are staggered. Time delays prior to switching the digital valves 60 to the OFF-state are not necessary.

One type of valve staggering control is a basic delay staggering. During the basic delay staggering a short delay is provided prior to the actuation of certain digital valves 60. The valve switching module 108 identifies which of the digital valves 60 to immediately actuate and which to delay. For example, when the shock absorber includes four digital valves, the valve switching module 108 may immediately actuate two of the digital valves 60, followed by the other two after a short delay. Accordingly, the valve switching module 108 may predefine the digital valves 60 that are to be delayed.

With reference to FIG. 9, an example of the basic delay staggering is presented. The graph illustrates switching from damping state 1 to states 2-16. The right side of the graph

illustrates the valve position for the digital valves 60 defined in FIG. 6. For example, in FIG. 6, the ON-state is represented by "1" and the OFF-state is represented by "0". Accordingly, for state 1, the valve state is "0000". Similarly, for state 4, the valve state is "0011". In the four digit binary valve, values from left to right represent the valve state of #1-digital valve 60, #2-digital valve, #3-digital valve, and #4-digital valve. Thus, for state 4, #1-digital valve 60 and the #2-digital valve 60 are in the OFF-state (i.e., "00") and the #3-digital valve 60 and the #4-digital valve 60 are in the ON-state (i.e., "11").

As shown in FIG. 9, if the present state is state 1 (0000) and the target state is state 7 (0110), #2-digital valve 60 is actuated first, then after a small delay, #3-digital valve 60 is actuated. Based on the basic delay staggering, one transient state is provided between the present and target state. Meaning, from the present state (0000) to the target state (0110), the damping state changes from 0000 (present state) to 0100 (transient state) to 0110 (target state). Per FIG. 9, a transient state is used in about 80% of the possible transition scenarios.

Another type of valve staggering control is a smart delay staggering. Similar to the basic delay staggering, the smart delay staggering provides a short delay prior to actuation of certain valves. However, in the smart delay staggering identification of which digital valves 60 to immediately actuate is determined based on which of the digital valves 60 need to be switched to achieve the target state. In other words, unlike the basic delay staggering, the valve switching module 108 does not predefine the digital valves to delay. The valve switching module 108 determines which valves are to be actuated based on the present state and the target state, and actuates one or more digital valves first, followed by other digital valves after the short delay if needed.

With reference to FIG. 10, an example of the smart delay staggering is presented. In particular, FIG. 10 illustrates switching from state 1 to states 2-16. In the example, the first and the second digital valves 60 that need to be switched are actuated immediately, followed by the third and fourth valves after the short delay. For example, if the present state is state 1 (0000) and the target state is state 12 (1011), the valve switching module 108 determines that #1, #3, and #4 digital valves 60 are to be actuated to reach state 12 (1011).

Using the smart delay staggering, #1 and #3 digital valves 60 are actuated first, and after a short delay, the #4 digital valve is turned on. The smart delay staggering may create one transient state in between the present and the target state if needed. Meaning, from the present state (0000) to the target state, such as state 12, the damping state changes from 0000 (present state) to 1010 (transient state) to 1011 (target state). As shown in FIG. 10, an intermediate state is used in about one third of the possible transition scenarios.

The flow area of the digital valves 60 may be used to define which digital valve 60 is to be delayed (the basic delay staggering) and/or which digital valve 60 is to be actuated based on the target state (smart delay staggering). Accordingly, for the basic staggering, the digital valves 60 that have the smaller flow area may be identified by the valve switching module 108 as the digital valves 60 to delay. Similarly, when the smart delay staggering determines the digital valves 60 that are to be actuated to reach the target state, the digital valves 60 that have the larger flow area are actuated first followed by the digital valves 60 with the smaller area.

As another variation, the valve staggering control may include a flow-area staggering. Flow-area staggering is similar to the smart delay staggering in that it determines which digital valves 60 are to be actuated based on the target state. Flow-area staggering also progresses the actuation of the digital valves 60 to be actuated from the digital valve 60 with

the largest flow area to the digital valve 60 with the smallest flow area and providing short delays in between actuation of each digital valve 60. Flow-area staggering provides for the lowest peak current requirement because only one valve is switched at a time.

With reference to FIG. 11, an example operation of the flow-area staggering method is presented. The example of FIG. 11 illustrates switching from state 1 to states 2-16. Based on the flow-area staggering method, the digital valve 60 with the largest flow area that needs to be switched is actuated immediately, followed sequentially by the other digital valves 60 after short delays. For example, if the present state is state 1 (0000) and the target state is state 8 (0111), the valves switching module 108 determines that #2, #3, and #4 digital valves 60 are to be actuated to reach the target state. Under the flow-area staggering method, the #2-digital valve 60 is actuated first. After a small delay, #3-digital valve 60 is actuated followed by, after a small delay, #4-digital valve 60.

Accordingly, between the present state and the target state, the damping state enters two transient states. Meaning, the damping state changes from 0000 (present state) to 0100 (transient state) to 0110 (transient state) to 0111 (target state). Based on FIG. 11, up to three transient states can be created between the present state and the target state.

A digital valve that is actuated first may be referenced as a primary valve and a digital valve that is actuated after the primary valve may be referenced to as a non-primary valve or secondary valve. It is readily understood that the digital valves may be switched or actuated in one or more groups with a delay disposed between each group.

In addition to valve staggering control, the switching methods provided by the valve switching module 108 may also include state transition control. State transition control may be used in parallel with valve staggering control. Multiple state transition controls described herein may also be used together. One of the goals of the state transition control is to optimize response time and NVH. State transition control, like valve staggering control, also uses additional states and delays; however the delays can be substantially longer. For instance, delays may be between 5-100 milliseconds for state transition control.

Without the state transition control, the damping state is switched immediately to the target state. In other words, there is no transition control in this mode. One type of state transition control is the fixed-step control in which the damping state transitions from the present state to the target state in a fixed number of steps defined by "m" where m is an integer. Accordingly, to transition from the present state to the target state, the transient state is every mth state.

With reference to FIG. 12, an example operation of the fixed-step control is illustrated. In FIG. 12, the present state is provided as state 3, and the target state is state 13. If there is no fixed state size (i.e., immediate switch), the damping state is switched immediately from state 3 to state 13. If the m=4, the damping state changes to every fourth state. Thus, from state 3 the damping state changes to state 7, then to state 11 before reaching the target state of state 13.

Under the fixed-step control, a determination may be made to ensure that the target state is not passed. For example, the fixed-step control may determine if the number of damping states between a present damping state and the target damping state is less than the fixed number of steps (m). If it is, the fixed-step control adjusts the damping state to the target state. Accordingly, when m=4, the damping state was switched from state 11 to the target state of state 13. In addition, as the fixed number of steps decreases, the time in which it takes to

reach the target state from the present state increases. Thus, the delay between the present state and the target state varies in the fixed-step control.

Another type of state transition control is a fixed transition time. In the fixed transition time, switch from the present state to the target state is performed in a preset amount of time. In other words, the time taken to reach a target state from a present state is the same regardless of the target state. For example, FIG. 13 illustrates the fixed transition time for different target states. In the example shown, the present state is state 3, and different lines shows the transition to a different target state, such as states 5, 8, 13, and 16. Based on the graph, the time taken to reach state 5 from state 3 is approximately the same as from state 3 to state 16.

Various switching methods, as described herein, can be used with the fixed transition time to determine which transient states are used to reach the target state within the fixed transition time. For example, the valve staggering controls, as described above, may be used to switch from the present state to the target state within the fixed transition time.

The state transition control also includes an overdrive control. Under the overdrive control, a damping state that is beyond the target state is provided as the transient state, and following a delay, the damping state is switched to the target state. One of the goals of the overdrive control is to achieve a faster hydraulic response. For example, FIG. 14 illustrates two overdrive controls. If the present state is state 3 and the target state is state 13, the fast overdrive control switches from state 3 (present state) to 16 (transient state) to 13 (target state). For the slow overdrive control, the damping state switches from 3 (present state) to 16 (transient state) to 15 (transient state) to 14 (transient state) to 13 (target state).

Accordingly, the overdrive control switches the damping state to a state beyond the target state before switching to the target state. In addition, the time in which the overdrive control performs the switch may be preset to allow for the fast or slow control.

The state transition control further includes a PID control. The PID control is based on known proportional-integral-derivative algorithms that calculate an error value as the difference between the target state and the present state. Also known as classical PID control, the number of transient states is based on the sum of calculations of the proportional, integral, and derivative values of the error. Individual multipliers ("gains") for proportional, integral, and derivative terms are used as the PID control. FIG. 14 illustrates a PID control for switching from state 3 (present state) to state 13 (target state).

Similar to classical PID, the state transition control also includes a quadratic control. The quadratic control uses a quadratic multiplier term consisting of the square of the error between the target state and the present state. The quadratic multiplier term replaces the derivative term. Quadratic control may be referred to as PIQ control. Quadratic transition control is meant to be a performance improvement to linear proportional control by using larger state changes with larger errors and smaller state changes with smaller error values. FIG. 14 illustrates the quadratic control for switching from state 3 (present state) to state 13 (target state).

The state transition control also includes an asymmetric control in which switching delays are set separately for the increasing and decreasing directions of damping state transitions. For example, FIG. 15 provides four examples in which the asymmetric control is used to transition between state 3 and state 13. In examples 1 and 3, the time taken to transition from state 13 to state 3 is less than the time taken to transition from state 3 to state 13. Whereas in examples 2 and 4, the time taken to transition from state 13 to state 3 is more than the time

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taken from state 3 to state 13. For performing the asymmetrical control, the valve switching module **108** may include a predefined logic table that defines the switching delays for the increasing and decreasing directions of damping state transitions.

In the examples provide thus far of the state transition controls, the transition between the present state to the target state includes switching to a discrete damping state. As part of the state transition controls, a fractional stepping control (i.e., pulse mode operation) creates a virtual position between the discrete damping states. The pulse mode operation creates the virtual positions by pulse modulation or fast switching between two positions.

One way to implement the pulse mode operation is by repeating the actuation pulse without the corresponding hold current applied. Specifically, the virtual position between two discrete damping states (i.e., two adjacent damping states) can be created by operating one or more valves in between the "OFF" and "ON" valve states. This can be achieved with pulse mode operation by oscillating between the "OFF" and "ON" valve states. The new states may be referred to as fractional states.

Another method involves pulse width modulation (PWM) control which is similar to micro-stepping in a stepper motor. Half stepping or micro-stepping with finer resolution is possible. PWM control is used as a transient method to improve NVH. Continuous pulse mode operation may generate excessive heat and power consumption. Pulse mode operation may be used in parallel with other state transition controls such as fixed step, PID, or quadratic control, as illustrated in FIG. **16**.

In addition to valve staggering control and state transition, the valve switching module **108** may include other switching methods for improving the performance of the shock absorber **20**. For example, in a synchronization control, a delay may be provided before turning off a hold current or before the actuation current pulse. Accordingly, the timing of hydraulic pressure discontinuities created by actuation of other digital valves or turning off other digital valves is matched or synchronized.

In a repeat actuation control, an actuation current pulse is applied to a coil associated with a digital valve **60** that is already intended to be in the ON-state. Repeat actuation control ensures that the target damper state is set. Specifically, there is a possibility that the digital valve **60** may not engage or stay in the ON-state due to, for example, excessive electromagnetic interference, contamination, high viscosity oil associated with low temperatures, low viscosity oil associated with high temperatures, and/or very high acceleration impact from an external source such as driving through a pothole. Accordingly, the repeat actuation control performs as a mitigating action for preventing a fault.

As a form of repeat actuation control, an actuation current pulse may be periodically applied to the digital valve **60** that is to be in the ON-state. For example, the valve switching module **108** may have the coil activation module periodically apply the actuation current based on a preset timer. The periodic application of the actuation current should be done sparingly to avoid generation of extra heat. For example, the preset timer may be set in the range of every 1-100 seconds.

As a form of repeat actuation control, an actuation current pulse can be applied when the measured temperature is above or below preset values. Such a control ensures that the shock absorber is performing at the intended damping state during extreme high or low temperature operation. For example, the temperature may be the temperature of the shock absorber, the fluid within the shock absorber a temperature of the housing in which the damper module **100** is disposed, or a com-

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bination of temperatures that indicate the temperature at which the shock absorber is performing. Temperature based repeat actuation might be in the range of every 1-100 seconds.

As a form of repeat actuation control, an actuation current pulse can be applied when the measured or calculated acceleration exceeds a preset value. Such a control ensures that the shock absorber **20** is set at the intended damping state following an impact load. For example, the acceleration may be provided by an accelerometer disposed at or near the shock absorber **20** and/or may be a combination of accelerations. One or more actuation pulses may be applied to each coil following a high acceleration.

The valve switching module **108** may also include warm-up controls to electrically heat the coils, valves, and oil at low temperatures. For example, an actuation current pulse may be applied when the measured temperature is below a preset value. The purpose is to generate additional heat to warm the digital valve **60** and the fluid within the shock absorber **20**. The actuation current pulse may be applied in the range of every 5-500 milliseconds.

As another form of the warm-up control, a continuous maximum (un-modulated) current may be applied when the measured temperature is below the preset value. Alternatively, the hold current (or another modulated current level) without the actuation pulse may be applied when the measured temperature is below the preset value.

A vehicle-level staggering delay may be used to reduce the peak current requirement. In other words, the shock absorbers **20** disposed at the corners of the vehicle can be controlled, such that the shock absorbers **20** do not switch at the same time to their respective damping states. One method of performing such control is by adding a short time delay between the commands sent by the master module **102** to each of the shock absorbers **20**. Staggering delays might typically be 1-2 milliseconds. Commands may be delayed to individual corner shock absorbers of the vehicle or commands may be sent in sets of two. For example, sets of two may consist of the two front suspension **14** shock absorbers **20** and the rear suspension **12** shock absorbers **20**.

The damper module **100**, which includes the valve switching module **108** and the coil activation module **110**, may use one or more of the switching methods described herein for actuating the digital valves **60**. For example, the damper module **100** may include a set of algorithms and/or predefined tables that define the switching method to be used for actuating the digital valves.

While the switching methods were described with regard to a shock absorber having four digital valves **60**, it is within the scope of this disclosure to apply the switching methods to shock absorbers having two or more digital valves **60**.

With reference to FIG. **17**, a flowchart of an example method **200** for performing a valve switching operation is presented. The damper module **100**, at **202** determines whether the damper setting has been received. For example, the damper module **100** may receive the damper setting from the master module **102**. If the damper setting has not been received, the damper module returns to **202**. If the damper setting has been received, the damper module **100** determines the target state (target damping state) of the shock absorber **20** based on the damper setting at **204**.

At **206**, the damper module **100** determines whether the present state is equal to the target state. If the present state is equal to the target state, the damper module **100** continues to **208**. If the present state is not equal to the target state, the damper module **100** performs a predefined switching method to change the present state to the target state at **210**. The switching method can be any one or more of the switching

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methods described above. For example, the switching method may be a combination of the smart delay staggering and the asymmetric control. After the switching method, the damper module 100 returns to 202.

At 208 the damper module 100 may maintain the power supply to the digital valves 60. For example, if digital valve 60 is in the second position a hold current may be applied to maintain the digital valve 60 in the second position. Although not shown, when maintaining the digital valves 60 at the present damping state, the damper module 100 may periodically actuate the digital valves that are in the second position. For example, the damper module 100 may perform a warm-up control to increase the temperature of the damper system, as described herein. The damper module 100 may also perform the repeat actuation control to ensure the digital valves 60, which are supposed to be in the second position, are in the ON-state. From 208, the damper module 100 returns to 202.

The foregoing description of the embodiments has been provided for purposes of illustration and description. It is not intended to be exhaustive or to limit the disclosure. Individual elements or features of a particular embodiment are generally not limited to that particular embodiment, but, where applicable, are interchangeable and can be used in a selected embodiment, even if not specifically shown or described. The same may also be varied in many ways. Such variations are not to be regarded as a departure from the disclosure, and all such modifications are intended to be included within the scope of the disclosure. In this application, including the definitions below, the term module may be replaced with the term circuit.

The term module may refer to, be part of, or include an Application Specific Integrated Circuit (ASIC); a digital, analog, or mixed analog/digital discrete circuit; a digital, analog, or mixed analog/digital integrated circuit; a combinational logic circuit; a field programmable gate array (FPGA); a processor (shared, dedicated, or group) that executes code; memory (shared, dedicated, or group) that stores code executed by a processor; other suitable hardware components that provide the described functionality; or a combination of some or all of the above, such as in a system-on-chip.

Example embodiments are provided so that this disclosure will be thorough, and will fully convey the scope to those who are skilled in the art. Numerous specific details are set forth such as examples of specific components, devices, and methods, to provide a thorough understanding of embodiments of the present disclosure. It will be apparent to those skilled in the art that specific details need not be employed, that example embodiments may be embodied in many different forms and that neither should be construed to limit the scope of the disclosure. In some example embodiments, well-known processes, well-known device structures, and well-known technologies are not described in detail.

The terminology used herein is for the purpose of describing particular example embodiments only and is not intended to be limiting. As used herein, the singular forms “a,” “an,” and “the” may be intended to include the plural forms as well, unless the context clearly indicates otherwise. The terms “comprises,” “comprising,” “including,” and “having,” are inclusive and therefore specify the presence of stated features, integers, steps, operations, elements, and/or components, but do not preclude the presence or addition of one or more other features, integers, steps, operations, elements, components, and/or groups thereof. The method steps, processes, and operations described herein are not to be construed as necessarily requiring their performance in the particular order discussed or illustrated, unless specifically

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identified as an order of performance. It is also to be understood that additional or alternative steps may be employed.

When an element or layer is referred to as being “on,” “engaged to,” “connected to,” or “coupled to” another element or layer, it may be directly on, engaged, connected or coupled to the other element or layer, or intervening elements or layers may be present. In contrast, when an element is referred to as being “directly on,” “directly engaged to,” “directly connected to,” or “directly coupled to” another element or layer, there may be no intervening elements or layers present. Other words used to describe the relationship between elements should be interpreted in a like fashion (e.g., “between” versus “directly between,” “adjacent” versus “directly adjacent,” etc.). As used herein, the term “and/or” includes any and all combinations of one or more of the associated listed items.

Although the terms first, second, third, etc. may be used herein to describe various elements, components, regions, layers and/or sections, these elements, components, regions, layers and/or sections should not be limited by these terms. These terms may be only used to distinguish one element, component, region, layer or section from another region, layer or section. Terms such as “first,” “second,” and other numerical terms when used herein do not imply a sequence or order unless clearly indicated by the context. Thus, a first element, component, region, layer or section discussed below could be termed a second element, component, region, layer or section without departing from the teachings of the example embodiments.

Spatially relative terms, such as “inner,” “outer,” “beneath,” “below,” “lower,” “above,” “upper,” and the like, may be used herein for ease of description to describe one element or feature’s relationship to another element(s) or feature(s) as illustrated in the figures. Spatially relative terms may be intended to encompass different orientations of the device in use or operation in addition to the orientation depicted in the figures. For example, if the device in the figures is turned over, elements described as “below” or “beneath” other elements or features would then be oriented “above” the other elements or features. Thus, the example term “below” can encompass both an orientation of above and below. The device may be otherwise oriented (rotated 90 degrees or at other orientations) and the spatially relative descriptors used herein interpreted accordingly.

What is claimed is:

1. A damper system for a vehicle comprising:

a shock absorber having a plurality of digital valves, wherein each of the plurality of digital valves is controllable to a first position or to a second position, and the shock absorber is operable at one of multiple damping states based on the plurality of digital valves; and

a damper module electrically coupled to each of the digital valves and controlling each of the digital valves to a desired position based on a damper setting received from a master module, the damper module applying an actuation current pulse for switching the digital valve from the first position to the second position, wherein the desired position is either the first position or the second position, the damper module determines a target damping state of the shock absorber based on the damper setting, the target damping state is one of the multiple damping states, and the damper module performs a switch operation to control the plurality of digital valves to a given desired position when the target damping state is different from a present damping state.

2. The damper system of claim 1 wherein the damper module predefines each of the digital valves as either a pri-

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mary valve or a secondary valve, and the digital valve, as the secondary valve, is switched from the first position to the second position after the primary valve is switched from first position to the second position and after a preset time period has lapsed.

3. The damper system of claim 1 wherein

the damper module determines whether at least one of the plurality of digital valves are to be switched from the first position to the second position based on the present damping state and the target damping state, and

when one digital valve from among the plurality of digital valves is to be switched, the damper module switches the one digital valve from the first position to the second position, and

when more than one digital valve from among the plurality of digital valves is to be switched, the damper module switches a primary valve from among the more than one digital valves from the first position to the second position, and switches a non-primary digital valve from the more than one digital valves from the first position to the second position after the primary valve and after a preset time period has lapsed, the primary valve has a flow area larger than the non-primary digital valve.

4. The damper system of claim 1 wherein

each of the plurality of digital valves are defined as a primary valve or a secondary valve, and the digital valve, as the primary valve, has a flow area larger than the secondary valve, and

the damper module determines which of the plurality of digital valves are to be switched from the first position to the second position based on the present damping state and the target damping, and when more than one digital valve is to be switched from the first position to the second position, the damper module switches the one or more digital valve one digital valve at a time with a preset time period disposed between each switch, and when the more than one digital includes the primary valve, the primary valve is switched before the secondary valve.

5. The damper system of claim 1 wherein the switch operation includes a staggering control and a state transition control, the staggering control generates a time delay between a primary valve and a secondary valve, such that the primary valve is switched from the first position to the second position before the secondary valve, and the state transition control switches one or more of the digital valves such that the shock absorber operates at a transient damping state prior to operating at the target damping state, the transient damping state is one of the multiple damping states different from the target damping state and present damping state, the primary valve and the secondary valve are among the plurality of digital valves.

6. The damper system of claim 1 wherein the master module is disposed in the vehicle separate from the damper module.

7. The damper system of claim 1 wherein the damper module utilizes a quadratic control as the switch operation when the present damping state is different from the target damping state.

8. The damper system of claim 1 wherein the damper module periodically applies the actuation current pulse to a subject digital valve from among the plurality of digital valves that is already in the second position.

9. The damper system of claim 1 wherein the damper module applies the actuation current pulse to a subject digital

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valve from among the plurality of digital valves that is in the second position when a temperature of the shock absorber is below a preset threshold.

10. The damper system of claim 1 wherein the shock absorber includes N number of digital valves as the plurality of digital valves, N is an integer, and the shock absorber has 2^N number of damping states as the multiple damping states.

11. The damper system of claim 1 wherein the damper module applies a hold current pulse to maintain a subject digital valve from among the plurality of digital valves in the second position, and deactivates the hold current pulse to switch the subject digital valve from the second position to the first position.

12. The damper system of claim 1 wherein the damper module applies a reverse current pulse to switch a subject digital valve from among the plurality of digital valves from the second position to the first position.

13. The damper system of claim 1 wherein the damper module applies the actuation current pulse to a subject digital valve from among the plurality of digital valves that is in the second position when an acceleration of the shock absorber is greater than or equal to a preset threshold.

14. A damper system for a vehicle comprising:

a shock absorber having a plurality of digital valves, wherein each of the plurality of digital valves has a valve state as either an ON-state or an OFF-state, and the shock absorber is operable at one of multiple damping states based on the valve state of the plurality of digital valves; and

a damper module electrically coupled to each of the digital valves and controlling each of the digital valves to a desired state based on a damper setting received from a master module, wherein the damper module determines a target damping state of the shock absorber based on the damper setting, the target damping state is one of the multiple damping states, the damper module controls the valve state of the plurality of digital valves to a given desired state to operate the shock absorber at the target damping state.

15. The damper system of claim 14 wherein the damper module includes a predefined switching logic to operate the shock absorber from a first damping state to a second damping state different from the first damping state, the first damping state and the second damping state are among the multiple damping states, the predefined switching logic controls the plurality of digital valves such that a time period for switching from the first damping state to the second damping state is different from a time period for switching from the second damping state to the first damping state.

16. The damper system of claim 14 wherein when the present damping state is different from the target damping state, the damper module controls the plurality of digital valves to operate the shock absorber at a transient damping state prior to operating the shock absorber at the target damping state, the transient damping state is one of the multiple damping states different from the target damping state and the present damping state.

17. The damper system of claim 14 wherein the transient damping state is set as one of the multiple damping states beyond the target damping state, such that when the target damping state is greater than the present damping state, the transient damping state is set to be greater than the target damping state, and when the target damping state is less than the present damping state, then the transient damping state is set to be less than the target damping state.

18. The damper system of claim 14 wherein the damper module controls the digital valves to operate the shock

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absorber at a transient damping state prior to operating the shock absorber at the target damping state, the transient damping state is between two adjacent damping states of the multiple damping states and is different from the target damping state and the present damping state.

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19. The damper system of claim 14 wherein the damper module controls the plurality of digital valves to operate the shock absorber at multiple transient damping states prior to operating the shock absorber at the target damping state, the multiple transient damping states are among the multiple damping states and are different from the target damping state and the present damping.

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20. The damper system of claim 14 wherein the damper module controls the plurality of digital valves based on a preset logic table that defines switching delays for transitioning from a first damping state to a second damping state different from the first damping state, the switching delays defined controls the plurality of digital valves such that a time period for switching from the first damping state to the second damping state is different from a time period for switching from the second damping state to the first damping state.

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UNITED STATES PATENT AND TRADEMARK OFFICE
CERTIFICATE OF CORRECTION

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APPLICATION NO. : 14/191885
DATED : December 22, 2015
INVENTOR(S) : Scott Dunaway et al.

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:


In the Specification:

At column 12, line number 39, delete "20" and insert --20.--.

In the Claims:

At column 15, claim number 9, line number 66, after "wherein", delete "t".

Signed and Sealed this
Twenty-third Day of August, 2016

A handwritten signature in black ink, reading "Michelle K. Lee". The signature is written in a cursive style with a large, stylized "M" and "L".

Michelle K. Lee
Director of the United States Patent and Trademark Office